

Figure 1 consists of 12 histograms arranged in a single column. Each histogram represents the frequency distribution of the number of non-zero elements in the vector x for a specific value of n . The x-axis for all histograms is 'Number of non-zero elements in x ' with major ticks at 0, 20, 40, 60, 80, 100, and 120. The y-axis is 'Frequency' with major ticks at 0, 20, 40, 60, 80, and 100. The histograms are labeled with n values: 10, 20, 30, 40, 50, 60, 70, 80, 90, 100, 110, and 120. As n increases, the distribution becomes more concentrated around the value n , and the peak frequency increases.

The major drawback of these devices lies in the fact that they are
35 severely disturbed by external illumination such as the street lighting or the

headlamps of other vehicles. The measurements taken by the photocells also depend strongly on the more or less reflecting nature of the surfaces illuminated in front of the vehicle. The setting obtained under these conditions is therefore not constant, and suffers substantial deviations depending on the environment of the vehicle.

It has been proposed, for example in the document FR-A-2 759 043, to remedy these drawbacks by proposing an installation for setting up the illumination range of the headlamps of a vehicle, comprising a transmission installation which transmits at least one beam of electromagnetic rays falling on a region to the front of the vehicle, an electro-optical detection installation which gives an image point, at least of the irradiated region, an interpretation installation which interprets the position of at least one irradiated region, and produces a signal from it which is compared with a datum signal representing the correct setting of the illumination range, and, in the event of a deviation between the actual signal and the datum signal, setting-up installations are driven so as to cancel out this deviation.

Such an installation, even if it solves the problem of the stray illumination and of the surface states of the road surfacing, nevertheless exhibits drawbacks. This is because the measurements taken by this installation amounts to analysing the movement of a spot of light on the ground in front of the vehicle. It will therefore be understood that, for a constant attitude of the vehicle, the measurements will be disturbed by the variation in the height of the vehicle, that is to say during movements of simultaneous compression or of expansion of all the elements of the suspension of the vehicle, which impart pure vertical-translation movements on the chassis of the vehicle. During such vertical-translation movements, the light spot in front of the vehicle moves, and this is all the more so the further the illuminated area is from the vehicle. The movement of the light spot is then interpreted by the interpretation installation as a change in attitude, the latter then generating an erroneous correction signal for the setting-up installations.

Summary of the invention

The present invention falls within this context, and its object is to propose a device for automatic correction of the orientation of the headlamps of a motor vehicle in elevation upon variations in the attitude of the vehicle, which do not require the installation of wheel sensors nor their wiring, which is insensitive to variations in the height of the vehicle, which is simple to implement and reliable, while being inexpensive.

Thus the subject of the present invention is a device for automatic correction of the orientation of at least one motor-vehicle headlamp upon variations in the attitude of the motor vehicle, including

- 5 - an emitter projecting, onto the ground in front of the vehicle, two light spots which are spaced apart in a direction parallel to the longitudinal axis of the vehicle,
- a sensor of the illumination of the light spots comprising an objective forming an image of the light spots on a receiver and supplying an output signal for each one,
- 10 - processing means suitable for deriving a control signal from the output signal from the sensor, and
- an actuator controlled by the control signal and able to alter the elevation orientation of a reflector of the headlamp.

According to the present invention, the control signal for the actuator is
15 derived by the processing means on the basis of a linear function of the output signals supplied by the sensor for each image of each light spot.

According to other advantageous and non-limiting characteristics of the invention:

- 20 - the linear function between the output signals from the sensor for each image of each light spot is of the form $dc_1 - a \times dc_2 = K \times (\theta - \theta_0) + b$, where a , b and θ_0 are constants characteristic of the geometry of the correction device, θ is an angle representative of the attitude of the vehicle, and where K is a magnitude representative of the height of the vehicle;
- the emitter and the sensor are fixed with respect to one another;
- 25 - the emitter and the sensor are integral with a movable part of the vehicle;
- the movable part of the vehicle consists of the reflector of a headlamp of the vehicle;
- the emitter and the sensor are fixed with respect to the vehicle;
- 30 - the emitter and the sensor are situated one on a fixed part of the vehicle, the other on a movable part of the vehicle;
- the light spots define a straight-line segment substantially parallel to the longitudinal axis of the vehicle;
- the emitter and the sensor are situated substantially in the same
35 vertical plane;

- the direction of illumination of the emitter and the optical axis of the sensor are contained in the same vertical plane parallel to the longitudinal axis of the vehicle.

Brief description of the drawings

5 Other objects, characteristics and advantages of the present invention will emerge clearly from the description which will now be given of an embodiment example given in a non-limiting way by reference to the attached drawings, in which:

- Figure 1 represents a diagrammatic view of the front of a vehicle
10 illustrating the principle of the invention according to a first embodiment;

- Figure 2 represents a theoretical operating diagram of the correction device according to the first embodiment;

- Figure 3 represents, in graphical form, the signal delivered by the sensor equipping the device of the invention;

15 - Figure 4 represents an example of an array of curves derived by the processing means equipping the device of the invention;

- Figure 5 represents a diagrammatic view of the front of a vehicle illustrating the principle of the invention according to a second embodiment;

- Figure 6 represents a diagrammatic view of the front of a vehicle
20 illustrating the principle of the invention according to a third embodiment, and

- Figure 7 represents a general diagram of the operating principle of the correction device according to the present invention.

Description of the preferred embodiments

On Figure 1 has been represented, diagrammatically, the front of a
25 vehicle V, equipped in a conventional way with headlamps P, a single headlamp having been represented. The headlamp P includes a reflector R interacting with a light source S integral with the latter so as to form a light beam for illuminating the road in front of the vehicle V. In the event that the headlamp P is intended to send out a dipped beam, the reflector R could be of the type able by itself to
30 generate a beam with cut-off, or be of the elliptical type, being integral with a converging lens the object focus of which is co-incident with one of the foci of the elliptical reflector the other focus of which is situated in the immediate vicinity of the light source S.

In the embodiment of Figure 1, an emitter 1 is integral with the
35 reflector R, as is a sensor 2. The emitter 1 projects two light spots T₁ and T₂ onto

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the ground in front of the vehicle V at different distances d_1 and d_2 , the spots T_1 and T_2 defining a straight-line segment parallel to the longitudinal axis of the vehicle. These spots T_1 and T_2 are situated in the field of view C of the sensor 2. The emitter 1 and the sensor 2 are situated substantially in the same vertical plane
5 parallel to the longitudinal axis of the vehicle, and the direction of illumination from the emitter 1 and the optical axis of the sensor 2 are contained in this plane, for example the plane of the Figure 1.

Upon changes in attitude by the vehicle V, the spots T_1 and T_2 move on the ground, these movements being observed by the sensor 2, which delivers a
10 corresponding signal, this signal being supplied to processing means 5, for example a computer or a microprocessor, which determine whether a correction to the orientation of the headlamp is necessary. If so, a command signal is generated by the computer 5 so as to steer an actuator 4 in one direction or another. The actuator 4 is situated in the housing B of the headlamp P and causes the reflector R to tilt
15 about a fixed point PF of the housing B, which alters the inclination of the reflector R, and therefore that of the light beam generated by it. With the emitter 1 being integral with the reflector R, the movement of the latter entails the movement of the spots T_1 and T_2 on the ground, which is observed by the sensor C.

The tilting of the reflector continues until the spots T_1 and T_2 occupy
20 their reference position with respect to the horizontal, and corresponding to a correct inclination of the light beam, despite the change in the attitude of the vehicle. The correction of the elevation orientation of the headlamp P can thus be obtained dynamically, this correction being performed in closed loop.

More precisely, as has been represented in Figure 2, the emitter 1,
25 placed at a height H above the road, sends out two pencil light beams L_1 and L_2 so as to form the spots T_1 and T_2 on the road in front of the vehicle, at distances d_1 and d_2 from the vertical of the emitter 1. The sensor 2, placed at a height h above the emitter 1, comprises an objective 3 forming, from the spots T_1 and T_2 , images I_1 and I_2 on a photosensitive surface 6. The objective 3 defines the optical axis C of
30 the sensor.

The emitter 1 and the sensor 2 are integral with one another and with the reflector R. The sensor 1 therefore measures the attitude of the reflector R. The emitter 1 and the sensor 2 are oriented in such a way that, when the orientation of the reflector R is the regulation or nominal orientation, the optical axis C of the
35 sensor intercepts the road at a point M situated at a distance d_m from the vertical of

the emitter 1, substantially in the middle of the straight-line segment lying between the spots T_1 and T_2 . The spots T_1 and T_2 are seen by the sensor in directions C_1 and C_2 . The optical axis C forms an angle θ with the road, and the pencil beams L_1 and L_2 form angles $(\theta-k_1)$ and $(\theta-k_2)$ with the road, k_1 and k_2 being the angles formed respectively between L_1 and C , and between L_2 and C .

The objective 3 of the sensor 2 can be analysed as being equivalent to a converging lens, with focal length f . This objective 3 forms, on the photosensitive surface 6, images I_1 and I_2 of the spots T_1 and T_2 , these images I_1 and I_2 being respectively at distances dc_1 and dc_2 from the centre m of the surface 6, corresponding to the intersection between the surface 6 and the optical axis C .

Geometric considerations make it possible to determine the distances dc_1 and dc_2 . Thus these formulae are obtained:

$$dc_1 = f \times \frac{-H \times \tan(k_1) \times \tan^2(\theta) + h \times \tan(\theta) - (h+H) \times \tan(k_1)}{(h+H) \times \tan^2(\theta) - h \times \tan(k_1) \times \tan(\theta) + H} \quad (1)$$

$$dc_2 = f \times \frac{-H \times \tan(k_2) \times \tan^2(\theta) + h \times \tan(\theta) - (h+H) \times \tan(k_2)}{(h+H) \times \tan^2(\theta) - h \times \tan(k_2) \times \tan(\theta) + H} \quad (2)$$

It is possible, moreover, to determine the constants k_1 and k_2 , characteristic of the specific geometry of the device used, such that:

$$\tan(k_1) = \frac{d_{10} \times (h+H_0) - H_0 \times d_{m0}}{H_0 \times (h+H_0) + d_{10} \times d_{m0}} \quad (3)$$

and

$$\tan(k_2) = \frac{d_{20} \times (h+H_0) - H_0 \times d_{m0}}{H_0 \times (h+H_0) + d_{20} \times d_{m0}} \quad (4)$$

where d_{10} , d_{20} , d_{m0} and H_0 are the nominal initial values of d_1 , d_2 , d_m and H . These nominal initial values are obtained for an unloaded vehicle, the inclination of the headlamp P being correctly set up.

It emerges clearly from the formulae (1) and (2) that dc_1 and dc_2 are functions only of the height H of the emitter 1, and consequently of the vehicle, and of the angle θ of inclination of the sensor 2 with respect to the road, and consequently of the attitude of the vehicle.

The photosensitive surface 6 on which the images I_1 and I_2 are formed advantageously consists of a linear CCD array (charge-coupled elements). When the elements of this array are scanned by the appropriate electric means, the signal obtained is of the form which is represented in Figure 3, each image I_1 and I_2

situated at the distance dc_1 and dc_2 from the sensor m of the surface 6 giving rise to a voltage spike at the instants t_1 and t_2 . The signal of Figure 3 includes, for example, a periodic negative pulse, of period T , at the instants t_0+nT , and positive pulses at the instants t_1 and t_2 .

5 The signal of Figure 3 is supplied to the processing means 5 which, for each scan, calculate, from t_1 and t_2 , the values of dc_1 and dc_2 , functions of the height H and of the angle θ as was seen above.

In accordance with the present invention, the processing means 5 derive a linear function of dc_1 and dc_2 , of the form:

$$10 \quad dc_1 - a \times dc_2 = K \times (\theta - \theta_0) + b \quad (5)$$

where θ_0 is the nominal initial value of the angle θ , obtained for an unloaded vehicle with a headlamp P correctly set up in inclination, and having the value:

$$\tan(\theta_0) = \frac{h + H_0}{dm_0} \quad (6)$$

where a and b are constants, of the form:

$$a = \frac{1 - \tan(k_1) \times \tan(k_2) + (\tan^2(\theta_0) - 1) \times \frac{\tan(k_1)}{\tan(\theta_0)}}{1 - \tan(k_1) \times \tan(k_2) + (\tan^2(\theta_0) - 1) \times \frac{\tan(k_2)}{\tan(\theta_0)}} \quad (7)$$

$$b = f \times \frac{\tan(k_2) - \tan(k_1)}{1 - \tan(k_1) \times \tan(k_2) + (\tan^2(\theta_0) - 1) \times \frac{\tan(k_2)}{\tan(\theta_0)}} \quad (8)$$

and where K is a function of the height H of the emitter 1.

15 Formula (5) is written:

$$dc_1 - a \times dc_2 = b \quad (9)$$

for the nominal initial value θ_0 of the angle θ , and no longer depends on the height H of the emitter 1. It follows that all the curves of equation (5) pass through the same point for the nominal initial value θ_0 of the angle θ , as has been represented in

20 Figure 4, whatever the height H of the emitter 1.

As can be seen in Figure 4, about the nominal initial position (θ_0, H_0) , the value of the equation (5) is very little dependent on the value H of the height of the emitter 1. It is therefore sufficient for the processing means 5 to calculate the value of the equation (5) and to compare the result with the constant b as defined by the relationship (8). The result of this comparison indicates the direction in which the headlamp P should be actuated:

- if $dc_1 - a \times dc_2 = b$, the headlamp is correctly set up, the processing means 5 do not send out any signal,

- if $dc_1 - a \times dc_2 < b$, that means that the angle θ is less than the nominal initial angle θ_0 , and that the beam sent out by the headlamp P is too high. The processing means 5 then send out a control signal for the actuator 4, so that the latter inclines the headlamp P further downwards, and

- if $dc_1 - a \times dc_2 > b$, that means that the angle θ is greater than the nominal initial angle θ_0 , and that the beam sent out by the headlamp P is too low. The processing means 5 then send out a control signal for the actuator 4, so that the latter inclines the headlamp P further upwards.

In the last two cases, as long as $dc_1 - a \times dc_2 \neq b$, the processing means send out a control signal proportional to the absolute value of the difference $(dc_1 - a \times dc_2) - b$, until this absolute value is equal to zero. The actuator 4 is then driven proportionally to the size of the correction to be applied to the inclination of the headlamp P. It results therefrom that the correction will be carried out all the more rapidly, which is important in order to reduce any dazzling of the other drivers in the case of a light beam which is too high.

Thus a device has actually been implemented for automatic correction of the orientation of motor-vehicle headlamps in elevation upon variations in attitude of the vehicle. The control signals sent out by the processing means 5 for the correction of the headlamp P could be used by a second actuator 4' placed in the housing of the other headlamp P' of the vehicle in order simultaneously to correct the orientation of the two headlamps by the use of a single automatic-correction device, or each headlamp of the vehicle could be equipped with its own automatic-correction device. The device according to the present invention does not require any wiring in the vehicle other than for its installation in the housing of the headlamp. The device corrects the orientation of motor-vehicle headlamps in elevation only upon variations in attitude of the vehicle, and it is insensitive to the variations in height of the vehicle.

Such an automatic-correction device is simple to implement and reliable. This is because it suffices to arrange an emitter, a sensor and an actuator in the housing of the headlamp P, these components all being well known and fully understood, and means for processing the signal generated by the sensor, which can amount to no more than a suitably programmed microprocessor. The electrical links between these various components are short, and contained completely in the

housing of the headlamp. Moreover, the linear function which the processing means use to generate the control signal for the actuator 4 involves two constants a and b, which are themselves calculated on the basis of the constants d_{10} , d_{20} , d_{m0} and H_0 , the nominal initial values of d_1 , d_2 , d_m and H , and geometric constants h and f of the device.

If the nominal initial values and the geometric constants of the device are known with precision, it is then easy to calculate the constants a and b theoretically, and to store them in the processing means 5, for example in an erasable and programmable read-only memory, of the EEPROM type.

If the nominal initial values and the geometric constants of the device are not known, or are known with insufficient precision, it is possible to determine the constants a and b experimentally. To do that, it is sufficient to observe the distances dc_1 and dc_2 of the images I_1 and I_2 of the spots T_1 and T_2 on the photosensitive surface 6 for two specific positions of the vehicle, for example the nominal initial position (vehicle unloaded, inclination of the headlamp correctly set up) and an extreme position (vehicle fully loaded, inclination of the headlamp correctly set up).

It is then possible to proceed in the following way:

- the orientation of the headlamps of the vehicle is set up manually, the automatic-correction device being inhibited;
- the distances of the images I_1 and I_2 of the spots T_1 and T_2 on the photosensitive surface 6 are measured, the vehicle being unloaded, and therefore in nominal initial position, the distances measured then being equal to dc_{10} and dc_{20} ;
- the distances of the images I_1 and I_2 of the spots T_1 and T_2 on the photosensitive surface 6 are measured, the vehicle being fully loaded, the distances measured then being equal to their minimum value $dc_{1, \min}$ and $dc_{2, \min}$;

$$- a \text{ is calculated, } a = \frac{dc_{10} - dc_{1, \min}}{dc_{20} - dc_{2, \min}} ;$$

$$- b \text{ is calculated, } b = dc_{10} - a \times dc_{20}, \text{ and}$$

a and b are stored in the processing means 5, for example in an erasable and programmable read-only memory, of the EEPROM type.

These settings, measurements and calculations can advantageously be carried out at the end of the motor-vehicle production line, when the vehicle is completely fitted out and ready to be delivered. The reference angle θ used for the measurements can be taken with respect to an axis different from the optical axis of

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the sensor 2, but situated in the field of view of the latter, if the settings, measurements or calculations are thereby facilitated.

This is because, in considering another reference axis, the distances of the images I_1 and I_2 of the spots T_1 and T_2 on the photosensitive surface 6 are slightly offset by a value Δ , so that they become: $dc'_1 = dc_1 + \Delta$ and $dc'_2 = dc_2 + \Delta$.
 5 The relationship (5) is then written:

$$dc'_1 - a \times dc'_2 = K(\theta - \theta_0) + b + \Delta \times (1 - a) \quad (10)$$

and all the calculations mentioned above can be repeated without change.

According to a second embodiment, represented in Figure 5, the emitter
 10 1 is installed on a fixed part of the vehicle, for example on the housing of the headlamp P or on a part of the vehicle itself, while the sensor 2 is integral with the reflector R, as in the preceding embodiment. A device installed in this way functions exactly as in the preceding embodiment. It requires only the addition of
 15 the sensor 2 with respect to the emitter 1. It would be possible, for example, to fit a recopy potentiometer PR in the vicinity of the fixed point PF on which the reflector R is articulated, the information output from this potentiometer being supplied to the processing means in order to correct the variation in the angle between the emitter 1 and the sensor 2.

20 According to a third embodiment, represented in Figure 6, the emitter 1 and the sensor 2 are both installed on a fixed part of the vehicle, for example both in the housing of the headlamp P. A device installed in this way functions exactly as in the first embodiment, and will therefore not be described in detail.

According to the three embodiments described above, it is quite clear
 25 that the relative positions of the emitter and of the sensor could be interchanged, the emitter 1 being located, for example, above the sensor 2. It results therefrom that a general diagram of the operating principle of the automatic-correction device according to the present invention can be drawn up, like the one which is represented in Figure 7.

30 A component E-R is seen in this figure, which can be an emitter or a receiver, and a component R-E, which can be a receiver or an emitter respectively. One is placed at a height H_1 , the other is placed at a height H_2 . They are arranged in vertical planes spaced horizontally by a fixed distance d . They exhibit a relative orientation represented by the angle δ , which is possibly variable. By way of the
 35 taking into account of the additional geometric constants d and δ , which are

characteristic of the device used, it is possible to follow the same reasoning and to re-write formulae (1) to (2) above, so as to arrive at a linear relation of the form:

$$dc_1 - a \times dc_2 = b$$

which it is appropriate to take into account between the positions dc_1 and dc_2 , on the photosensitive surface of the sensor, of the images I_1 and I_2 of the light spots T_1 and T_2 projected by the emitter.

It is thus possible to arrange the emitter or the sensor at any desired place on the vehicle, the emitter being arranged, for example, level with the headlamp or with the front bumper of the vehicle, while the sensor could be arranged in the passenger compartment, for example behind the rear-view mirror.

A device has therefore actually been produced for automatic correction, in real time, of the orientation of motor-vehicle headlamps in elevation, upon variations in attitude of the vehicle. It would be possible to use a single device for the two headlamps of the vehicle, in which case the control signals sent out by the processing means for the correction of the orientation of one headlamp could be used for the simultaneous correction of the orientation of the other headlamp of the vehicle. It would also be possible to use a correction device associated with each headlamp. According to the embodiments represented in Figures 1, 2, 5 and 6, the device does not require any wiring in the vehicle other than for its installation in the housing of the headlamp, which thus constitutes a self-contained unit with automatic correction incorporated. The device corrects the elevation orientation of motor-vehicle headlamps only upon variations in attitude of the latter, and it is insensitive to the variations in height of the vehicle.

Needless to say, the present invention is not limited to the embodiments which have been described, but the person skilled in the art, on the contrary, could apply numerous modifications to it which come within his scope. Thus, for example, it would be possible to use two emitters each projecting a light spot onto the ground. These two emitters will be integral with one another in such a way that the light spots are formed by light rays forming a constant and predetermined angle between them. It would be possible, for example, to use light-emitting diodes or laser diodes mounted on the same circuit, appropriate optics forming the emerging rays. The laser diodes will advantageously emit infra-red radiation. Likewise, provision could be made for the light spots to be emitted alternately, or for them to be emitted continuously, their intensity being modulated according to a predetermined law. It would also be possible to make provision to replace the CCD

or CMOS sensor with an analogue positioning circuit, of the PSD (Position Sensor Device) type.